

# Storage of Methane in Clathrate Hydrates: Monte Carlo Simulations of sI Hydrates and Comparison with Experimental Measurements

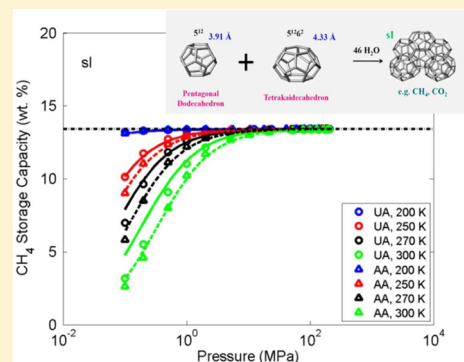
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## Supporting Information

**ABSTRACT:** Extensive grand canonical Monte Carlo simulations are performed for the calculation of the amount of methane gas that can be stored inside the hydrate structure sI focusing on temperature and pressure conditions that are of interest to practical applications (e.g., methane storage/transportation, methane hydrates in nature). Langmuir-type "absorption isotherms" are used in order to present the results for methane in the cages of the hydrate structure. In particular, the methane content inside the different type of hydrate cages is given as a function of pressure, where the parameters of this function are temperature-dependent. A comparison between available experimental data for cage occupancies and calculated values resulted in good agreement. The correlation between chemical potential and pressure is determined through NVT Monte Carlo simulations. Simulations are performed for the TIP4P/Ice water model and two methane models (United-Atom and All-Atom). The calculations of the current study can be utilized during the process of refining the estimates of methane gas "in-place", in hydrate deposits, when pressure and temperature conditions at the hydrate reservoirs are known. A discussion on the implication to geologic media containing hydrates is also presented.



## 1. INTRODUCTION AND BACKGROUND

Conditions of high pressures or low temperatures in the presence of water, within natural or artificial environments, are suitable for the formation of nonstoichiometric, crystalline materials that are known as clathrate hydrates. The water molecules can form, through hydrogen-bonding, different types of cages/cavities that can be stabilized by the presence of guest molecules of particular sizes that can fit within the cages. Commonly encountered types of cages in hydrate-related studies include the following: pentagonal dodecahedron ( $S^{12}$ ), tetrakaidecahedron ( $S^{12}6^2$ ), hexakaidecahedron ( $S^{12}6^4$ ), irregular dodecahedron ( $4^35^66^3$ ), and icosahedron ( $S^{12}6^8$ ). Different combinations of cage-types and cage-numbers can produce the building blocks (unit cells) for the three most common (i.e., sI, sII, and sH) hydrate structures.<sup>1</sup>

As a result of the discovery of large amounts of methane ( $CH_4$ ) hydrates during the recent years in natural, geologic environments (e.g., inside oceanic sediments at the continental slopes, and at the Arctic permafrost regions), hydrates are currently considered possible future energy sources.<sup>2–4</sup> Preliminary estimates<sup>5–7</sup> of the total amount of  $CH_4$  gas that is stored in hydrate deposits are encouraging and thus make the study of  $CH_4$  hydrates very attractive, even though the total amount of stored  $CH_4$  gas is still under debate within the scientific community.

On the other hand, the natural occurrence of  $CH_4$  inside the geologic hydrate deposits can have a significant impact on the

environment. In particular, if  $CH_4$  is released abruptly in the atmosphere, it can contribute significantly to the global warming<sup>8,9</sup> because  $CH_4$  is a "greenhouse" gas that has a higher heat-trapping ability than  $CO_2$  and, therefore, a stronger effect on the global warming problem.

Of particular industrial importance is the characteristic of hydrates to store large amounts of gas within their crystalline structure. Consequently, they have been under consideration for industrial applications of storing and transporting "energy-carrier" gases (e.g.,  $CH_4$ <sup>10–12</sup> and  $H_2$ <sup>13,14</sup>).

The accurate knowledge of the storage capacity of  $CH_4$  hydrates is a fundamental question that needs to be answered in order to utilize hydrates for industrial applications. Reliable answers can be obtained by either experimental measurements or computational calculations. Experimental approaches have been developed<sup>15–25</sup> and have reported the measured  $CH_4$  content in hydrates. Circone et al.<sup>20</sup> reported a detailed discussion on experimental issues and difficulties that are related to measuring the gas composition of hydrates. On the other hand, grand canonical Monte Carlo (GCMC) simulations<sup>26</sup> (i.e., constant chemical potential, volume, and

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temperature) have been considered a low-cost alternative methodology to calculate the gas content of hydrates. This methodology has been used extensively to study  $H_2$  storage in hydrates.<sup>27–30</sup> The method has the important advantage of allowing the occupancy in each type of cavity, present in the hydrate structure, to be calculated separately. The application of the particular methodology to mixtures of  $CH_4$  with other gases (e.g.,  $CO_2$ ) is rather straightforward. This issue is of particular interest to studies related to gas mixture separation processes. A number of studies have been reported that use MC simulations for  $CH_4$  hydrates.<sup>31–43</sup>

Significant attention from industry and academia has been shown toward  $CH_4$  hydrates resulting from their importance. Areas of primary interest include: flow assurance issues in oil/gas flow lines<sup>44</sup> that result from hydrate formation, the in situ formation of  $CH_4$  hydrate in naturally occurring porous media,<sup>45–54</sup> and  $CH_4$  production during hydrate dissociation within geologic formations.<sup>55–63</sup>

The primary focus of the current study is the calculation of the  $CH_4$  storage capacity (i.e.,  $CH_4$  content) of structure sI hydrate, over a wide temperature (200–300 K) and pressure (0.1–220 MPa) ranges, using a MC simulation approach. We report Langmuir-type mathematical functions for the cavity occupancies,  $\theta_i$  (with  $i = S, L$ , where S denotes the small cage, and L the large cage), as a function of pressure,  $P$ , and temperature,  $T$ :  $\theta_i = f(P, T)$ . Once such mathematical expressions for the cavity occupancies, as a function of pressure and temperature, become available, then we can calculate the  $CH_4$  content for any given pressure and temperature. These equations can be used for the interpolation and extrapolation of the derived simulation data but also can be useful for predicting the  $CH_4$  content in other hydrate systems (e.g., hydrates with promoters). Moreover, such analytical expressions could be used for the prediction of hydrate equilibrium (e.g., van der Waals–Platteeuw theory<sup>64</sup>), where the relation between occupancies and fugacity (pressure) is usually required as an input.

The particular issues that are of interest to the current study have also been examined in an earlier work,<sup>35</sup> where preliminary results have been reported. However, the current study provides additional new insight with regard to four different aspects, when compared to the earlier study. In particular: (i) in the current study, we use an elaborate and self-consistent approach based on MC simulations in order to relate the chemical potential and pressure of the system, whereas in the earlier study, a more crude approach was utilized that was based on the use of equations of state, (ii) in the current study, we examine a model for water that has been shown to produce more accurate calculations during molecular dynamics simulations, (iii) a more extensive comparison with experimental and computational studies is included in the current study, and finally, (iv) a discussion is provided that examines the effects of pressure on the storage capacity of naturally occurring hydrates, particularly for cases when the pressure within the deposit is significantly higher than the equilibrium pressure. This issue is of significant importance because it can affect the total amount of  $CH_4$  present in the deposit; therefore, it can affect the discussion on the economic viability of  $CH_4$  production from a particular hydrate deposit.

The current study is organized as follows: A brief background on hydrates and the water and  $CH_4$  models used are initially presented. Next, we describe the simulation details. Then, the results from the MC simulations are presented, and

subsequently, their comparison with available experimental data and other computational studies is discussed. Finally, a discussion on the implication to geologic media containing hydrates also is presented that is followed by the conclusions.

## 2. METHODOLOGY

**2.1. Hydrate Structure.** For the current study, the simulation box consists of 27 unit cells,  $(3 \times 3 \times 3)$ , of sI hydrate. It contains 1242 water molecules that form a total of 54 small ( $S^{12}$ ) and 162 large ( $S^{12}6^2$ ) cavities. The space group symmetry ( $Pm3n$ ) of the hydrate crystal has been determined from XRD measurements.<sup>65</sup> The atomic positions are taken from the work of Takeuchi et al.<sup>66</sup> and correspond to those proton configurations that have (almost) zero dipole moment among all possible configurations that obey the so-called “ice rules”.<sup>67</sup> The lattice constant (12.03 Å) for the sI hydrate has also been taken from Takeuchi et al.<sup>66</sup> Furthermore, we assume that the value of the lattice constant is kept constant for the entire pressure and temperature range and water molecules are kept rigid and at fixed positions throughout the simulation. The use of a flexible water lattice would increase the computational cost.

**2.2. Water and  $CH_4$  Models.** Water molecules in the current study are represented with the TIP4P/Ice<sup>68</sup> water model. The TIP4P/Ice is a rigid four-site model in which a LJ sphere is fixed on the oxygen site. The electrostatic contributions are implemented by positive partial charges located on each hydrogen atom and a negative partial charge fixed on an “M-site”, located on the bisector of the H–O–H angle at 0.1577 Å from the oxygen atom. The O–H bond length is 0.9572 Å and the H–O–H angle is 104.52°. Values for the LJ parameters and the charges are given in Table 1. The

**Table 1. Parameters of the Water Model Used in the GCMC Simulations**

model	site	$\sigma$ (Å)	$\epsilon$ (kJ/mol)	charge ( $e$ )
TIP4P/Ice <sup>68</sup>	O	3.1668	0.8822	0.0000
	H	0.0000	0.0000	+0.5897
	point M	0.0000	0.0000	−1.1794

TIP4P/Ice started attracting the attention of hydrate-related studies only recently, after it was initially identified as the most appropriate to predict accurately the three-phase hydrate equilibria using molecular dynamics<sup>69</sup> or MC simulations.<sup>34</sup> Subsequently, it has been used by other molecular simulation hydrate studies<sup>37–40,70–72</sup> as well.

Two different models are examined for the case of the  $CH_4$  molecule. In the first model, the  $CH_4$  molecule is represented as a single-interaction site (united-atom approach) that interacts via a 12–6 Lennard-Jones (LJ) potential. In particular, the OPLS–UA<sup>73</sup> model has been used for  $CH_4$ . Table 2 shows

**Table 2. Parameters of the  $CH_4$  Models Used in the GCMC Simulations**

model	site	$\sigma$ (Å)	$\epsilon$ (kJ/mol)	charge ( $e$ )	distance (Å) <sup>a</sup>	angle (°) <sup>a</sup>
OPLS–UA <sup>73</sup>		3.7300	1.2301	0.000	n/a	n/a
OPLS–AA <sup>74</sup>	C	3.500	0.27614	−0.240	$d_{C-H} =$	$\theta_{HCH} =$
	H	2.500	0.12552	+0.060	1.090	109.47

<sup>a</sup>n/a: not applicable.

the LJ parameters for both models. The net charge of the CH<sub>4</sub> molecule is zero, and consequently, there are no electrostatic interactions, neither between CH<sub>4</sub> molecules nor between CH<sub>4</sub> and water. For the second model, the OPLS-AA (all-atom)<sup>74</sup> has been used.

**2.3. Simulation Details.** In the current study, we have used the GCMC methodology that was originally developed by Metropolis et al.<sup>75</sup> All simulations were performed with the open-source package for Monte Carlo (MC) simulations MCCCSTowhee<sup>76</sup> (Version 7.1.0). In the simulations, a cutoff distance of 15 Å has been used for all types of interactions. LJ interaction parameters between different types of interacting sites were calculated with the Lorentz–Berthelot combining rules.<sup>26</sup> No tail corrections were applied to the LJ interactions. The Ewald summation<sup>26</sup> was used for the long-range electrostatic interactions. In addition, 3D periodic boundary conditions were applied to the simulation box.

Each run consisted of an equilibration stage of  $2 \times 10^6$  MC steps followed by a production stage of  $5 \times 10^6$  MC steps. In the GCMC runs, the following MC moves were applied with equal probabilities: insertion, destruction, rotation (used only for the case of OPLS-AA), and translation. One out of every 50 steps during the production stage ( $10^5$  steps in total) was taken into account for the average calculation of properties.

For the determination of the occupancy for each type of cavity, each CH<sub>4</sub> molecule was assigned to the cavity whose center was closest to the molecule's position. In this way, the average occupancy  $\theta$  (i.e., average number of CH<sub>4</sub> molecules per cavity) can be separately calculated for every cavity type. For a hydrate structure that contains  $k$  types of cavities and there are  $n_i$  cavities of type  $i$  together with  $n_w$  water molecules in the unit cell, the gas content, expressed as weight percentage (wt %), is given by

$$(\text{wt } \%) = \frac{\text{MW}_g \cdot \sum_{i=1}^k n_i \cdot \theta_i}{\text{MW}_g \cdot \sum_{i=1}^k n_i \cdot \theta_i + n_w \cdot \text{MW}_w} \cdot 100 \quad (1)$$

where  $\text{MW}_g$  and  $\text{MW}_w$  are the molecular weights of the guest gas and water, respectively. In the more general case where a promoter (i.e., help guest that contributes in hydrate formation under more favorable  $P$ ,  $T$  conditions) is also present in the hydrate structure, the term  $n_p \cdot \theta_p \cdot \text{MW}_p$  needs to be added to the denominator of eq 1, where it is assumed that the promoter has a molecular weight  $\text{MW}_p$  and occupies the cavities of type  $p$  with an average occupancy  $\theta_p$ . Usually, it is assumed that all of the promoter-designated cavities are fully occupied by one promoter molecule, therefore,  $\theta_p = 1$ .

### 3. RESULTS AND DISCUSSION

**3.1. Relation between Pressure and Chemical Potential of CH<sub>4</sub>.** The basic input of a GCMC run is the chemical potential of the “absorbate”, which can be calculated using the Widom insertion method.<sup>77</sup> In order to correlate the chemical potential with the pressure we performed a series of MC simulations of bulk CH<sub>4</sub> in the NVT ensemble, namely under constant number of CH<sub>4</sub> molecules ( $N$ ), volume ( $V$ ), and temperature ( $T$ ). In these NVT runs, a cubic simulation box was used. At every pressure value, the box volume was such that it contained at least 500 CH<sub>4</sub> molecules but its side length remained longer than double the cutoff distance (15 Å). In each run, the virial pressure was calculated

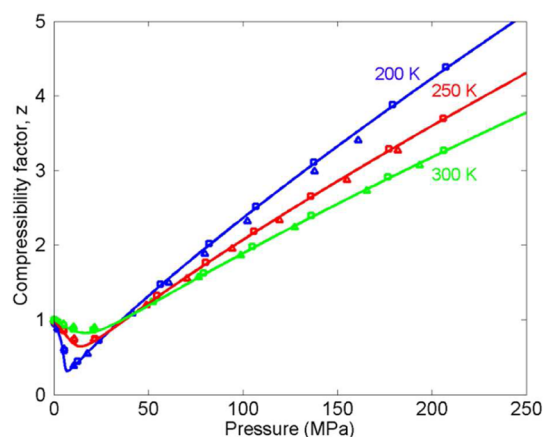
$$P = \frac{NkT}{V} - \frac{1}{3V} \sum_i \sum_{j>i} r_{ij} \frac{dU_{ij}}{dr} \quad (2)$$

The chemical potential was calculated with the Widom insertion method.<sup>77</sup> According to this method, after each MC step, an additional CH<sub>4</sub> molecule is randomly inserted in the simulation box and its potential energy  $U_{N+1}$  from the interactions with the rest of the molecules is calculated. The chemical potential  $\mu$  is given by the following equation:

$$\mu = \mu_0 - kT \ln \left\langle \exp \left( -\frac{U_{N+1}}{kT} \right) \right\rangle \quad (3)$$

where  $\langle \dots \rangle$  denotes average over all MC steps, and  $\mu_0$  is the ideal gas chemical potential. The reference value of chemical potential,  $\mu_0$ , is calculated from an additional NVT run where all interactions are set to zero. The chemical potential is calculated as a function of pressure, at constant temperature. This approach is more reliable and self-consistent than using a macroscopic equation of state (EoS), as has been done in previous studies.<sup>28–30,35</sup> However, it requires additional computational runs.

In this way, each run corresponds to a certain CH<sub>4</sub> density and for this density the pressure and chemical potential are calculated from eqs 2 and (3), respectively. This procedure not only allows the relation between pressure and chemical potential to be determined but also provides the EoS for the examined gas. This is shown in Figure 1 together with an EoS

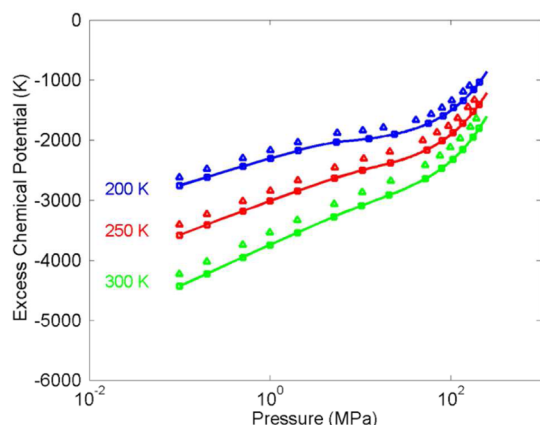


**Figure 1.** PVT behavior of CH<sub>4</sub> gas. Comparison between computational results (denoted with symbols; squares are UA, triangles are AA) obtained from NVT MC simulations with calculations from an experimental EoS<sup>78</sup> (denoted with lines). Confidence limits are smaller than the symbol sizes.

that has been directly fitted to experimental data for CH<sub>4</sub>.<sup>78</sup> Even at high pressures, there is very good agreement between the MC results and the experimental EoS.

The excess chemical potential as a function of pressure is shown in Figure 2 for three temperatures. The calculated values depend on the molecular model used for CH<sub>4</sub>. We observe that the OPLS-AA potential gives higher values than the OPLS-UA potential. However, this difference does not affect the results of the GCMC simulations since the chemical potential is converted to pressure according to the appropriate temperature-dependent curve in Figure 2. Shown also are the calculations with the accurate component-specific EoS.<sup>78</sup> The





**Figure 2.** Excess chemical potential ( $\mu^{\text{ex}}/k$ ) of  $\text{CH}_4$  gas as a function of pressure. MC data points are denoted with symbols (squares are UA, triangles are AA). Solid lines denote calculations with an experimental EoS.<sup>78</sup> Confidence limits are smaller than the symbol sizes.

calculations using the EoS and the OPLS-UA are in very good agreement.

### 3.2. Regression and Discussion of the MC Simulation Results.

In the current study, we performed an extensive series of GCMC simulations for structure sI  $\text{CH}_4$  hydrate. Simulation results are reported for the following four temperatures (isotherms): 200, 250, 270, and 300 K. The obtained MC results are reported in Tables S1–S8 of the [Supporting Information](#), along with the confidence limits of the simulations. It is evident that due to the large number of MC realizations used for the calculation of the properties the statistical uncertainties are very low. For the particular temperatures examined, the corresponding hydrate equilibrium pressures,  $P^{\text{eq}}(T)$ , that are calculated using CSMGem<sup>1</sup> are equal to 0.117, 1.162, 2.306, and 55.507 MPa, respectively. The pressure range considered in this study includes two distinct pressure zones. One high pressure zone where the hydrate is thermodynamically stable, [ $P^{\text{eq}}(T)$  – 220 MPa], and a second low pressure zone where the hydrate is thermodynamically unstable, [0.1 MPa –  $P^{\text{eq}}(T)$ ]. For the second pressure zone it is essential to assume that a hypothetical  $\text{CH}_4$  hydrate of structure sI exists and perform GCMC simulations in order to estimate the total amount of  $\text{CH}_4$  that the hypothetical structure can absorb. Simulations at the lower pressure zone are

essential only for the case of stabilizing the  $\text{CH}_4$  hydrate using a promoter. In that case the hydrate can be stable at significantly lower pressures. One should note, however, that the use of a promoter results in lower storage capacities since a fraction of cavities is occupied by the promoter.

Figure 3a and 3b show the cavity occupancy for the small and large cages respectively, that were obtained from the GCMC simulations of the sI  $\text{CH}_4$  hydrate, in the pressure range 0.1–220 MPa, and the considered series of isotherms. In the current study, we considered the entire pressure range for all the isotherm curves in order to be able to correlate the GCMC calculations for the cage occupancies  $\theta_s$  and  $\theta_L$ , using Langmuir-type curves. This is the traditional type of formulation that is used to describe the relation between cavity occupancy and fugacity or pressure.<sup>79,80</sup>

In particular, the GCMC results for the cage-occupancies,  $\theta_i$  (with  $i = S, L$ ), are fitted to the following type of curves:

$$\theta_i(P) = \frac{C_i(T) \cdot P}{1 + C_i(T) \cdot P} \quad (4)$$

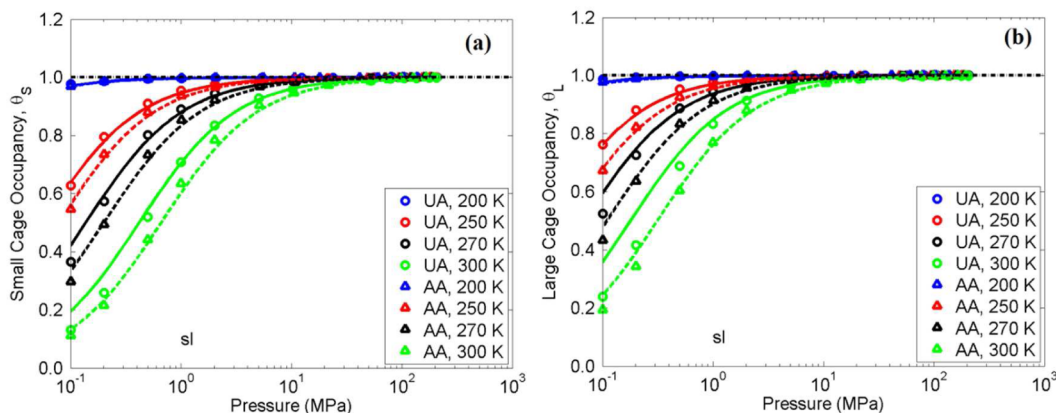
where the parameter  $C_i(T)$ , is temperature dependent and is given by the following equation:

$$C_i(T) = \frac{A_i}{T} \cdot \exp\left(\frac{B_i}{T}\right) \quad (5)$$

Note that eq 4 is theoretically founded only for cavities that can hold one guest molecule at most (i.e., single occupancy).<sup>1</sup> The adjustable parameters  $A_i$  and  $B_i$  are specific to each cavity type. The obtained optimum values for the set of parameters that describe the cavity occupancies resulting from the GCMC simulations are given in Table 3.

In Figure 3, the GCMC simulation results are denoted with symbols and the lines show the Langmuir-type isotherm-fitted curves. The GCMC results and the lines that are depicted with the same color correspond to the same temperature. Very good agreement between the GCMC results and the Langmuir-type curves, fitted to the GCMC simulation results, is obtained. Furthermore, the difference between the OPLS-UA and OPLS-AA is the direct result of the difference in the excess chemical potential shown in Figure 2.

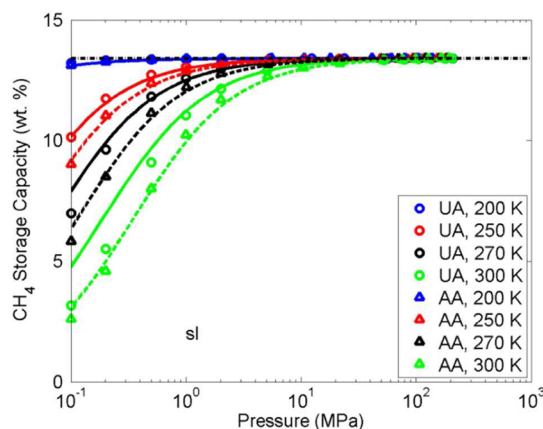
Figure 4 shows the  $\text{CH}_4$  storage capacity (i.e.,  $\text{CH}_4$  content of the hydrate structure), expressed as wt %, of the sI hydrate as a function of pressure in the pressure range [0.1–220] MPa



**Figure 3.** Cage occupancy obtained from GCMC simulations of sI  $\text{CH}_4$  hydrate in the pressure range (0.1–220) MPa, and various isotherms for (a) the small cages and (b) the large cages. Symbols denote the GCMC results and lines (solid is UA, dashed is AA) are the Langmuir-type isotherm-fitted curves. Isotherm info depicted with the same color. Confidence limits are smaller than the symbol sizes.

**Table 3.** Obtained Parameters for the Langmuir-Type Curves Describing the Cage Occupancies Resulting from the GCMC Simulations<sup>a</sup>

CH <sub>4</sub> model	parameter	small cavity $i = S$	large cavity $i = L$
OPLS-UA	$A_i$ (K/MPa)	$(63.8143 \pm 15.6340) \times 10^{-3}$	$(466.5032 \pm 115.7500) \times 10^{-3}$
OPLS-UA	$B_i$ (K)	$(27.8670 \pm 0.5233) \times 10^2$	$(24.3950 \pm 1.0292) \times 10^2$
OPLS-AA	$A_i$ (K/MPa)	$(27.3460 \pm 3.9900) \times 10^{-3}$	$(219.2944 \pm 30.4030) \times 10^{-3}$
OPLS-AA	$B_i$ (K)	$(29.1950 \pm 0.2404) \times 10^2$	$(25.2220 \pm 0.4514) \times 10^2$

<sup>a</sup>Uncertainty was estimated at the confidence level (90%).**Figure 4.** CH<sub>4</sub> storage capacity (wt %) as a function of pressure for the sI hydrate and for various isotherms. Symbols denote the GCMC simulation results and lines (solid is UA, dashed is AA) are those calculated from the Langmuir-type isotherm-fitted curves. Confidence limits are smaller than the symbol sizes.

and for the various isotherms. We examine pressures both below and above the hydrate equilibrium pressure. We observe that, for any given temperature, an increase at the pressure above the equilibrium value, results in the increase of the CH<sub>4</sub> content of the sI hydrate only by a limited amount. This is a direct result of the fact that the cages have already high occupancies at the hydrate equilibrium conditions. Therefore, no dramatic increase in the hydrate storage capacity can occur by increasing the pressure above the equilibrium value.

In addition, it is well known that the lattice constant of the CH<sub>4</sub> hydrate crystal depends on both the temperature and pressure.<sup>25,81</sup> However, as the MD study of Docherty et al.<sup>81</sup> showed, the change in the lattice constant for CH<sub>4</sub> hydrate at a temperature of 250 K and pressure range 3–200 MPa is approximately 0.6%. Therefore, given also that the CH<sub>4</sub> hydrate does not exhibit multiple cage occupancy and has also a high level of cage filling, we do not expect a significant effect of the lattice constant on the cavity occupancy results. Therefore, we consider the lattice constant fixed throughout all simulations reported in the current study.

**3.3. Comparison with Experiments and Other Computational Studies.** Figure 5 shows a comparison of the GCMC Langmuir-type fits with the experimental results of Uchida et al.<sup>16</sup> for the small and large cages. Uchida et al.<sup>16</sup> used Raman spectroscopy in order to measure the crystallographic hydration number,  $n_w$ , which gives the number of water molecules in the hydrate lattice per guest CH<sub>4</sub> molecule and is equal to  $n_w = \frac{46}{6\theta_L + 2\theta_S}$ . Uchida et al.<sup>16</sup> reported experiments in the temperature range 273.7–278.3 K, and pressure range 2.99–8.08 MPa.

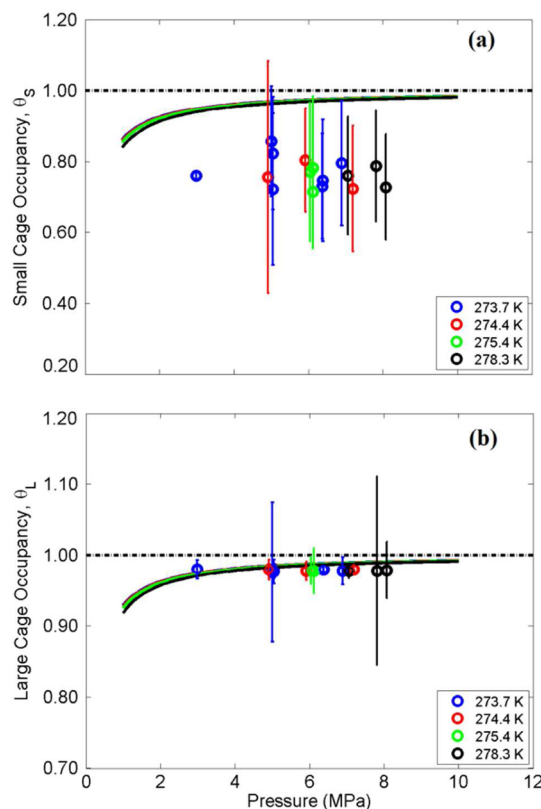
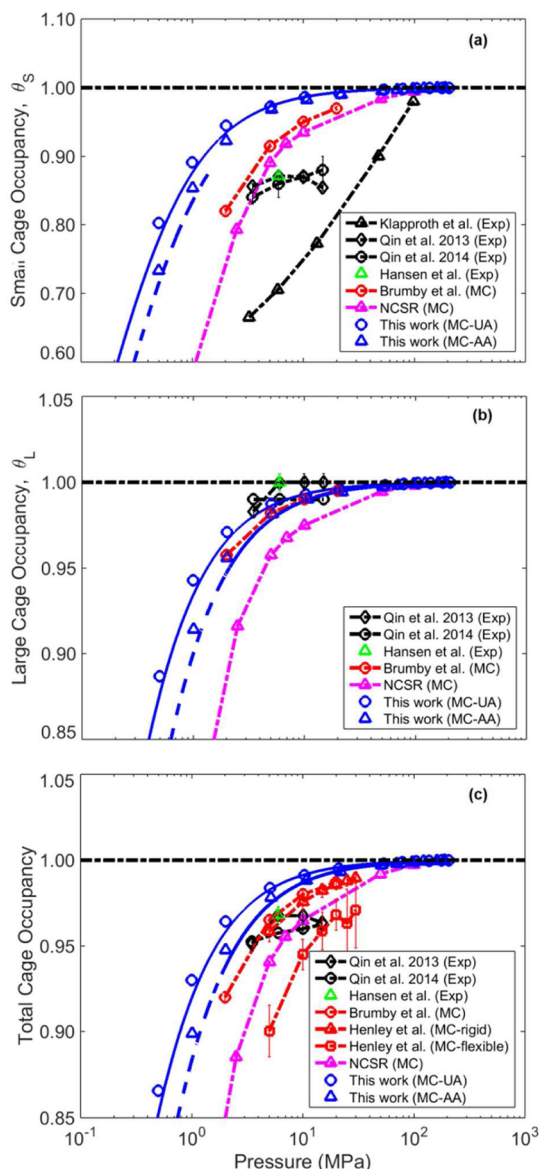
**Figure 5.** Cage occupancies as a function of pressure for (a) the small cages, and (b) the large cages and various temperatures. Comparison between the Langmuir-type fitted curve to the GCMC data (denoted with solid lines), and the experimental data of Uchida et al.<sup>16</sup> (denoted with circles).

Figure 5a refers to the cage occupancies for the small cages,  $\theta_S$ . The experimental data are plotted versus pressure, as a series of four isotherms, where we grouped the experimental data with similar temperatures and plotted them using an average temperature (i.e., 273.7, 274.4, 275.4, and 278.3 K). Figure 5a shows also the four Langmuir-type curves using the parameters obtained in the current study by fitting the GCMC simulations (Table 3). The four curves are very close to each other and overpredict, in general, the experimental data. Note, however, that all curves fall close to the upper bound of the experimental error that was reported by Uchida et al.<sup>16</sup> In Figure 5b, the cage occupancies for the large cages,  $\theta_L$ , are presented. For this particular case, the experimental data give an almost constant value for the large cage occupancy,  $\theta_L \approx 0.98$ , for all temperatures and pressures examined, implying an almost-complete cage occupancy. The GCMC Langmuir-type curves for the large cage occupancy exhibit a very good agreement with the reported experimental data.

Figure 6 shows a comparison of cage occupancies as a function of pressure for isotherms in the range 268–271 K. In



**Figure 6.** Cage occupancies plotted as a function of pressure for isotherms in the range 268–271 K for (a) the small cages, (b) the large cages, and (c) total cage occupancies. Blue lines (solid is UA; dashed is AA) denote the calculations using the Langmuir-type curves obtained from the current GCMC simulations. Dashed-dotted lines are guides to the eye only, connecting the corresponding experimental or earlier MC studies. NCSR denotes the GCMC simulations by Papadimitriou et al.<sup>35</sup> Confidence limits not shown are smaller than the symbol sizes.

particular, four sets of experimental data<sup>18,23–25</sup> are compared with recently reported MC simulation studies<sup>35,39,40</sup> as well as simulations from the current study. It should be noted that Klapproth et al.<sup>18</sup> reported experimental data only for the small cages at 271.15 K. The experimental data of Qin and Kuhs,<sup>23</sup> Qin et al.,<sup>24</sup> and Hansen et al.<sup>25</sup> are at 268 K. On the other hand, the GCMC simulations that were reported by Papadimitriou et al.<sup>35</sup> were performed at 273.15 K, whereas the current GCMC simulations are at 270 K. Henley and Lucia<sup>39</sup> performed Gibbs ensemble MC (GEMC) simulations

in order to calculate cage occupancies and reported values only for the total cage occupancy. They considered both a flexible and a rigid lattice. Their simulations, shown in Figure 6, correspond at a temperature equal to 270 K. Brumby et al.<sup>40</sup> also performed GEMC simulations at 270 K in order to calculate cage occupancies and results are shown in Figure 6. It should be noted that even though the studies are not at exactly the same temperature, the comparison is valid because within such a narrow temperature range the cage occupancies are not expected to change significantly. This behavior has been observed as well in Figure 5. The following conclusions can be reached:

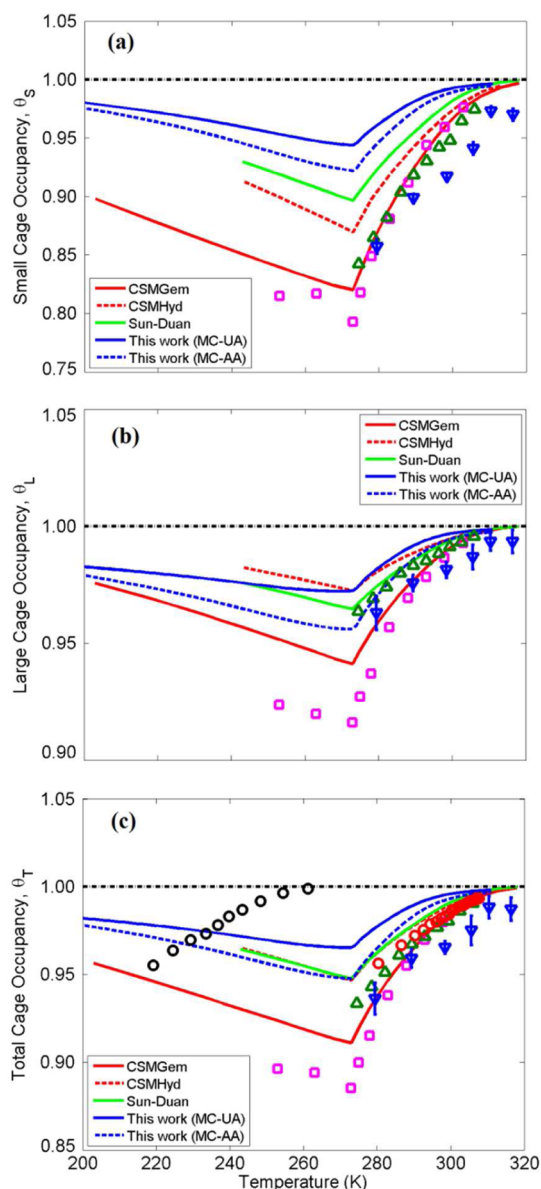
- The occupancies (i.e., small, large cages) reported by the earlier study by Papadimitriou et al.<sup>35</sup> are lower than the current study, primarily as a result of using a smaller lattice constant in the earlier study, and secondarily as a result of using SPC/E water model in the earlier study. In a recent study on H<sub>2</sub> hydrates,<sup>82</sup> it was found that the use of SPC/E water model resulted in lower occupancies compared to the case of TIP4P/Ice.
- The GCMC simulations of the current study and those using the GEMC simulations by Henley and Lucia<sup>39</sup> and Brumby et al.<sup>40</sup> are in very good agreement with the experimental large cage occupancies (Figure 6b).
- A less satisfactory agreement is observed for the case of the small cage occupancies with the simulations, resulting in higher occupancies than the experimental values. The GCMC simulations of the current study for the case of the small cages are also higher than the GEMC simulations (Figure 6a).
- The use of a flexible lattice can result in lower cage occupancies. This is clearly shown in Figure 6c, where the simulations with a flexible lattice by Henley and Lucia<sup>39</sup> resulted in lower total cage occupancies when compared with simulations using a rigid lattice as the current simulations or earlier studies.<sup>35,40</sup>

In Figure 7, we present the cavity occupancies, as a function of temperature, for the small cavities,  $\theta_s$  (Figure 7a), the large cavities,  $\theta_L$  (Figure 7b), and the total cavity occupancy of the hydrate unit cell,  $\theta_T$ , (Figure 7c) along the hydrate equilibrium curve  $P^{\text{eq}} = f(T)$ , for the sI CH<sub>4</sub> hydrates. Comparison is made for cavity occupancies calculated using the following three methods:

- The thermodynamic model of Sun and Duan<sup>80</sup>
- The commercial simulators CSMHyd<sup>83</sup> and CSMGem<sup>1</sup>
- The Langmuir-type fitted curves to the occupancy results obtained in the current study with the GCMC simulations

with reported results from MC simulations obtained by Papadimitriou et al.,<sup>35</sup> Jensen et al.,<sup>34</sup> and Ravipati and Punnathanam.<sup>41–43</sup> It should be noted that the simulations reported in the current study using TIP4P/Ice and the results of Papadimitriou et al. using SPC/E are based on the assumption that the three-phase  $P$ ,  $T$ , equilibrium conditions are known and calculating subsequently the cage occupancies at the known conditions. On the other hand, the studies of Jensen et al.<sup>34</sup> and Ravipati and Punnathanam<sup>41–43</sup> make an effort to calculate the three-phase equilibrium conditions. Therefore, the occupancy results correspond to the equilibrium conditions that are calculated by their methodology. The error in the calculation of the equilibrium temperature results in shifting the corresponding occupancy curves by several K. A more





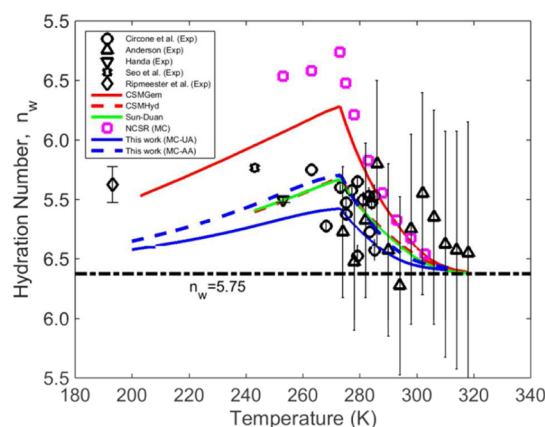
**Figure 7.** Calculated cage occupancies for sI CH<sub>4</sub> hydrates, along the hydrate equilibrium curve  $P^{\text{eq}} = f(T^{\text{eq}})$  for (a) the small cages,  $\theta_s$ , (b) the large cages,  $\theta_L$ , and (c) the total cage occupancy,  $\theta_T$ . Symbols denote MC simulations: magenta squares, Papadimitriou et al.;<sup>35</sup> blue triangles, Jensen et al.;<sup>36</sup> green triangles, Ravipati and Punathanam;<sup>43</sup> circles, Ravipati and Punathanam;<sup>43</sup> (black is SPC/E; red is TIP4P/Ice). Confidence limits for the MC simulations of Papadimitriou et al.<sup>35</sup> are smaller than the symbol sizes, whereas for the experimental data of Ravipati and Punathanam<sup>43</sup> are not available.

pronounced effect is observed in Figure 7c for the case of the results reported by and Ravipati and Punathanam<sup>43</sup> for the SPC/E water model. We observe that the corresponding equilibrium curve is shifted considerably toward the temperature range 220–260 K. SPC/E is known to underpredict significantly the melting point of ice (i.e., it predicts a melting point of ice equal to 214 K<sup>84</sup>), which is reflected, as well, in the calculation of the three-phase hydrate equilibrium. On the other hand, the results reported by and Ravipati and Punathanam<sup>43</sup> for the TIP4P/Ice water model, as well as, those by Jensen et al.<sup>34</sup> using the same model are closer to the calculations of the thermodynamic models that are considered for comparison. It should be noted that the TIP4P/Ice water

model is significantly more accurate in the calculation of the melting point of ice, predicting a value equal to  $270 \pm 3$  K.<sup>84</sup>

It should be noted that the models of Sun and Duan, CSMHyd, and CSMGem make use of the van der Waals–Platteeuw theory<sup>64</sup> coupled with an EoS. Good agreement is observed between the models of Sun and Duan and CSMHyd. A similar agreement is observed between the GCMC results of Papadimitriou et al.<sup>35</sup> and CSMGem. In general, CSMGem gives the lower values of all examined computational methods, whereas the current simulations with the OPLS–UA give the higher values.

Figure 8 shows a similar comparison between experimental and calculated values for the hydration number,  $n_w$ . The

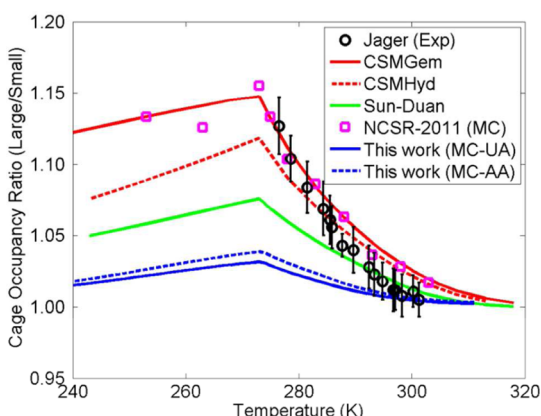


**Figure 8.** Hydration number,  $n_w$ , calculated using various approaches, and available experimental data for sI CH<sub>4</sub> hydrates along the hydrate equilibrium curve  $P^{\text{eq}} = f(T^{\text{eq}})$ . Confidence limits for the MC simulations of Papadimitriou et al.<sup>35</sup> are smaller than the symbol sizes, whereas for the experimental data of Seo et al.<sup>19</sup> are not available.

dashed-dotted line at the value of  $n_w = 5.75$  denotes the limiting case with 100% occupancy of both small and large cages. For this particular case, the experimental data of Circone et al.<sup>20</sup> are used for the higher  $T$ 's, whereas the experimental data of Handa<sup>21</sup> and Ripmeester et al.,<sup>22</sup> are used for the case of lower  $T$ 's. Shown also are the calculations reported by Anderson,<sup>85</sup> which are based on the Clapeyron equation. We observe that the results from all the examined calculation methods fall within the scatter of the experimental data. The scatter of the experimental data is also an indication of the complexity and difficulty of the measurements.

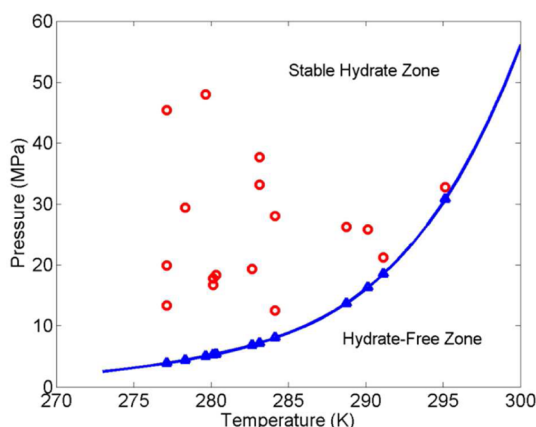
Figure 9 refers to the comparison of the calculated cavity occupancy ratio,  $\theta_L/\theta_s$ , with the experimental data of Jager<sup>17</sup> for sI CH<sub>4</sub> hydrates. It should be noted that the experimental data of Jager<sup>17</sup> are within the hydrate stability zone (i.e., for a given temperature the corresponding experimental pressure is a few bars higher than the hydrate equilibrium pressure, as calculated with the correlation reported by Moridis<sup>55</sup>). On the other hand, all the other calculations shown in Figure 9 were performed along the hydrate equilibrium curve  $P^{\text{eq}} = f(T)$ . We observe that the earlier GCMC simulations reported by Papadimitriou et al.<sup>35</sup> are in good agreement with the experimental data of Jager for the entire temperature range. On the other hand, the current GCMC simulations exhibit good agreement only for temperatures higher than approximately 288 K.

**3.4. Implication for Geological Conditions/Media.** It has been observed in various natural geologic environments (i.e., within oceanic sediments or permafrost areas) where CH<sub>4</sub>



**Figure 9.** Calculated cage occupancy ratio,  $\theta_L/\theta_S$ , and experimental data for sI CH<sub>4</sub> hydrates reported by Jager.<sup>17</sup> Confidence limits for the MC simulations of Papadimitriou et al.<sup>35</sup> are smaller than the symbol sizes.

hydrates have been discovered that the pressure is significantly higher than the hydrate equilibrium pressure<sup>86,87</sup> that corresponds to the temperature of the hydrate deposit. The three-phase equilibrium conditions are calculated in the current study through the correlation reported by Moridis.<sup>55</sup> This behavior is clearly demonstrated in Figure 10, where the



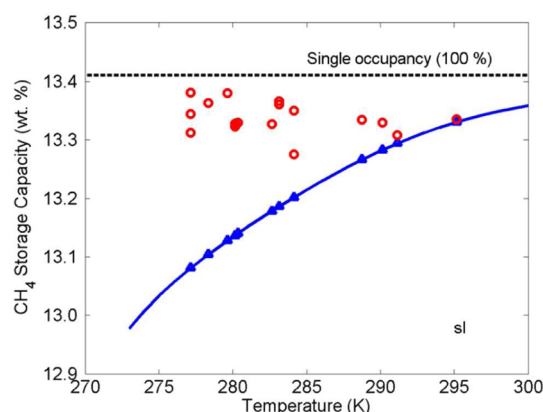
**Figure 10.** Prevailing  $P$ ,  $T$  conditions at various oceanic sites (denoted with circles) where hydrates have been identified (Makogan et al.<sup>86</sup>). The solid line corresponds to the CH<sub>4</sub> hydrate equilibrium curve  $P^{\text{eq}} = f(T^{\text{eq}})$ .<sup>55</sup> Triangles denote the corresponding equilibrium pressures for the  $T$  conditions of the particular oceanic sites.

prevailing pressure and temperature conditions of some known oceanic hydrate sites are plotted. It is evident from the figure that certain sites have pressures that are close to the hydrate equilibrium pressure (e.g., sites Guatemala-1 and Blake Ridge-2 in ref 86, where the names are indicative of the geographic location of the hydrate deposit), whereas others can have pressures that are approximately 41.5–43.0 MPa above the hydrate equilibrium pressure (e.g., sites Nankai-2 and Peru-Chile-1 in ref 86). The following two questions were raised by Papadimitriou et al.<sup>35</sup> for cases where the pressure within the geological sediments is higher than the hydrate equilibrium pressure:

- “Is the amount of CH<sub>4</sub> enclathrated in the hydrate increased when compared to the amount at the equilibrium conditions?”

- If the answer to the previous question is yes, then “By what percent does the storage capacity increase?”

Figure 11 shows the calculation of the CH<sub>4</sub> storage capacity using eq 1 coupled with the Langmuir-type fits of the GCMC



**Figure 11.** CH<sub>4</sub> storage capacity of sI hydrate (denoted with circles) calculated at the prevailing  $P$ ,  $T$  conditions at various oceanic sites where hydrates have been identified (Makogan et al.<sup>86</sup>). The solid line corresponds to the CH<sub>4</sub> storage capacity at  $P$ ,  $T$  conditions along the hydrate equilibrium curve  $P^{\text{eq}} = f(T^{\text{eq}})$ . Triangles denote the corresponding equilibrium storage capacities for the  $T$  conditions of the particular oceanic sites.

simulations for the cage occupancies. We observe a stronger effect at lower  $T$ 's as a result of the lower cage occupancies at three-phase equilibrium conditions. Therefore, an increase in the pressure above the three-phase equilibrium pressure can result in an increase of the cage occupancy, approaching the limiting value of 1 (i.e., single occupancy). However, as the temperature increases, the cage occupancies (at three-phase equilibrium conditions) approach the limiting value of 1. As a result, the cage occupancies cannot increase any further, even if the pressure increases significantly. For such cases in order to obtain any additional increase in the occupancy, upon pressure increase, would require double occupancy of cages. It should be noted, however, that such behavior has not been observed for the case of sI CH<sub>4</sub> hydrates. Multiple occupancy for CH<sub>4</sub> hydrates (equal to 3.1) has been observed only for the case of large cages ( $S^{12}6^8$ ) of sH CH<sub>4</sub> hydrates,<sup>88</sup> which are larger than the large cages ( $S^{12}6^2$ ) of sI CH<sub>4</sub> hydrates.

The maximum increase in CH<sub>4</sub> storage capacity for the cases examined was 2.3%, corresponding to the case of Nankai-2 oceanic site. The particular value may seem insignificant at first; however, we need to keep in mind that it is applied at the field-scale of geological settings, whose size can be of the order of kilometers. Therefore, overall it could contribute a significant amount to the overall energy recovery if the hydrate deposit is large. For the particular conditions of interest, both the OPLS-UA and OPLS-AA produce similar results.

#### 4. CONCLUSIONS

We have performed an extensive series of MC simulations on sI clathrate hydrates with CH<sub>4</sub> as the guest gas, over wide temperature (200–300 K) and pressure (0.1–220 MPa) ranges. It was found that the small and large cavities of sI hydrate structure cannot hold more than one CH<sub>4</sub> molecule, which is in good agreement with previous computational and experimental studies. Subsequently, we have developed simple



equations that correlate the occupancy of each hydrate cavity with temperature and pressure. These equations are Langmuir-type and give very good correlation of the simulation results. Such expressions can be useful in hydrate-related studies (e.g., three-phase equilibrium calculations based on the van der Waals–Platteeuw theory, storage capacities) where the dependence of cavity occupancy is explicitly required as an input. An extensive comparison is performed against available experimental data and computational studies with good agreement. Finally, the developed expressions have been utilized to examine the effect of pressure on the amount of CH<sub>4</sub> gas that is stored in naturally occurring hydrate deposits because a number of deposits are at pressure conditions that are significantly higher than the hydrate equilibrium pressure that corresponds to the temperature of the deposit.

## ■ ASSOCIATED CONTENT

### ■ Supporting Information

The Supporting Information is available free of charge on the ACS Publications website at DOI: 10.1021/acs.jced.6b00256.

Values with pressure and temperature conditions where simulations were performed, the obtained MC results, and the associated confidence intervals are reported in Tables S1–S8. (PDF)

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### Notes

The authors declare no competing financial interest.

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# Storage of Methane in Clathrate Hydrates: Monte Carlo Simulations of sI Hydrates and Comparison with Experimental Measurements

## Supporting Information

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## Monte Carlo Results

Each uncertainty was estimated at the confidence limit (95%).

Table S1. OPLS – UA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
200	0.100	-2752.4	0.9775	0.9870	0.0009	0.0007
200	0.200	-2614.7	0.9881	0.9934	0.0007	0.0005
200	0.502	-2434.5	0.9958	0.9973	0.0004	0.0003
200	1.010	-2301.0	0.9978	0.9986	0.0003	0.0002
200	2.038	-2173.1	0.9990	0.9993	0.0002	0.0002
200	5.391	-2027.4	0.9993	0.9997	0.0002	0.0001
200	12.374	-1971.1	0.9995	0.9998	0.0001	0.0001
200	23.711	-1896.4	0.9998	0.9998	0.0001	0.0001
200	56.300	-1716.1	0.9999	0.9999	0.0001	0.0000
200	82.010	-1594.8	1.0000	1.0000	0.0000	0.0000
200	106.861	-1456.2	1.0000	1.0000	0.0000	0.0000
200	137.455	-1339.1	1.0000	1.0000	0.0000	0.0000
200	179.156	-1156.7	1.0000	1.0000	0.0000	0.0000
200	207.510	-1032.3	1.0000	1.0000	0.0000	0.0000

Table S2. OPLS – AA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
200	0.100	-2613.6	0.9688	0.9778	0.0011	0.0009
200	0.201	-2475.8	0.9854	0.9890	0.0007	0.0006
200	0.503	-2295.2	0.9942	0.9955	0.0005	0.0004
200	1.011	-2161.1	0.9970	0.9977	0.0003	0.0003
200	2.052	-2031.5	0.9983	0.9988	0.0003	0.0002
200	5.539	-1879.1	0.9994	0.9995	0.0002	0.0001
200	10.623	-1830.9	0.9994	0.9995	0.0002	0.0001
200	17.947	-1784.5	0.9995	0.9997	0.0001	0.0001
200	41.447	-1659.5	0.9997	0.9998	0.0001	0.0001
200	60.797	-1564.0	0.9998	0.9999	0.0001	0.0001
200	79.969	-1454.5	0.9999	0.9999	0.0000	0.0001
200	102.601	-1333.1	1.0000	1.0000	0.0000	0.0000
200	137.901	-1182.1	1.0000	1.0000	0.0000	0.0000
200	161.065	-1085.5	1.0000	1.0000	0.0000	0.0000

Table S3. OPLS – UA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
250	0.100	-3579.3	0.6275	0.7624	0.0030	0.0026
250	0.200	-3406.7	0.7954	0.8808	0.0025	0.0020
250	0.501	-3179.5	0.9104	0.9531	0.0018	0.0013
250	1.005	-3009.4	0.9540	0.9762	0.0013	0.0009
250	2.018	-2842.6	0.9767	0.9874	0.0009	0.0007
250	5.127	-2633.6	0.9889	0.9947	0.0007	0.0005
250	10.537	-2495.6	0.9942	0.9970	0.0005	0.0003
250	21.603	-2378.0	0.9965	0.9980	0.0004	0.0003
250	54.524	-2160.5	0.9986	0.9991	0.0002	0.0002
250	80.338	-2010.4	0.9991	0.9997	0.0002	0.0001
250	105.873	-1871.7	0.9993	0.9998	0.0002	0.0001
250	135.933	-1715.6	0.9996	0.9999	0.0001	0.0001
250	177.366	-1520.9	0.9998	0.9999	0.0001	0.0001
250	205.991	-1404.3	1.0000	1.0000	0.0000	0.0000

Table S4. OPLS – AA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
250	0.100	-3405.9	0.5456	0.6719	0.0031	0.0029
250	0.200	-3233.1	0.7342	0.8223	0.0027	0.0024
250	0.502	-3005.4	0.8784	0.9251	0.0020	0.0016
250	1.007	-2834.5	0.9373	0.9625	0.0015	0.0012
250	2.031	-2666.0	0.9669	0.9807	0.0011	0.0009
250	5.211	-2451.8	0.9868	0.9917	0.0007	0.0006
250	10.895	-2304.7	0.9919	0.9954	0.0006	0.0004
250	21.335	-2185.2	0.9952	0.9971	0.0004	0.0003
250	49.116	-1995.7	0.9974	0.9988	0.0003	0.0002
250	70.585	-1871.4	0.9989	0.9992	0.0002	0.0002
250	94.445	-1760.0	0.9993	0.9995	0.0002	0.0001
250	119.517	-1628.7	0.9994	0.9997	0.0002	0.0001
250	155.155	-1449.0	0.9997	0.9999	0.0001	0.0001
250	182.129	-1328.8	0.9998	0.9999	0.0001	0.0001



Table S5. OPLS – UA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
270	0.100	-3917.5	0.3647	0.5252	0.0030	0.0031
270	0.200	-3730.8	0.5745	0.7265	0.0031	0.0028
270	0.501	-3485.0	0.8025	0.8868	0.0025	0.0020
270	1.004	-3300.5	0.8913	0.9428	0.0019	0.0014
270	2.015	-3118.7	0.9443	0.9709	0.0014	0.0010
270	5.097	-2887.7	0.9724	0.9874	0.0010	0.0007
270	10.374	-2727.9	0.9862	0.9930	0.0007	0.0005
270	21.155	-2584.9	0.9920	0.9960	0.0006	0.0004
270	53.688	-2345.3	0.9966	0.9983	0.0004	0.0003
270	79.143	-2186.2	0.9983	0.9990	0.0003	0.0002
270	105.497	-2043.4	0.9989	0.9995	0.0002	0.0001
270	136.936	-1884.4	0.9994	0.9997	0.0001	0.0001
270	177.535	-1697.1	0.9995	0.9998	0.0001	0.0001
270	206.554	-1546.1	0.9998	0.9999	0.0001	0.0001

Table S6. OPLS – AA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
270	0.100	-3730.2	0.2961	0.4332	0.0028	0.0031
270	0.200	-3543.4	0.4926	0.6357	0.0031	0.0030
270	0.501	-3297.1	0.7330	0.8331	0.0027	0.0023
270	1.006	-3111.8	0.8533	0.9141	0.0022	0.0017
270	2.027	-2928.2	0.9225	0.9559	0.0017	0.0013
270	5.168	-2692.1	0.9680	0.9814	0.0011	0.0008
270	10.761	-2523.7	0.9819	0.9903	0.0008	0.0006
270	22.025	-2372.6	0.9899	0.9943	0.0006	0.0005
270	50.986	-2155.0	0.9956	0.9975	0.0004	0.0003
270	69.697	-2045.3	0.9966	0.9983	0.0004	0.0003
270	97.117	-1899.0	0.9980	0.9991	0.0003	0.0002
270	122.338	-1752.5	0.9989	0.9994	0.0002	0.0001
270	160.244	-1580.0	0.9995	0.9997	0.0001	0.0001
270	187.855	-1448.8	0.9997	0.9998	0.0001	0.0001

Table S7. OPLS – UA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
300	0.100	-4431.6	0.1304	0.2388	0.0021	0.0026
300	0.200	-4224.1	0.2586	0.4163	0.0027	0.0031
300	0.501	-3950.3	0.5192	0.6894	0.0031	0.0029
300	1.003	-3744.4	0.7085	0.8331	0.0028	0.0023
300	2.010	-3540.4	0.8343	0.9141	0.0023	0.0017
300	5.060	-3277.6	0.9285	0.9642	0.0016	0.0012
300	10.241	-3089.0	0.9604	0.9810	0.0012	0.0008
300	20.814	-2911.8	0.9790	0.9897	0.0009	0.0006
300	52.474	-2638.0	0.9895	0.9957	0.0006	0.0004
300	79.213	-2467.6	0.9955	0.9974	0.0004	0.0003
300	105.044	-2316.2	0.9972	0.9984	0.0003	0.0002
300	136.168	-2156.2	0.9979	0.9991	0.0003	0.0002
300	176.870	-1949.4	0.9991	0.9995	0.0002	0.0001
300	206.219	-1802.1	0.9995	0.9997	0.0001	0.0001

Table S8. OPLS – AA					Uncertainty, $u$	
$T$ (K)	$P$ (MPa)	$\mu/k_b$ (K)	$\theta_{Small}$	$\theta_{Large}$	$\theta_{Small}$	$\theta_{Large}$
300	0.100	-4223.5	0.1102	0.1936	0.0019	0.0024
300	0.200	-4015.8	0.2139	0.3428	0.0025	0.0029
300	0.501	-3741.6	0.4407	0.6033	0.0031	0.0030
300	1.004	-3534.9	0.6343	0.7700	0.0030	0.0026
300	2.023	-3329.2	0.7846	0.8783	0.0025	0.0020
300	5.127	-3061.3	0.9043	0.9489	0.0018	0.0014
300	10.526	-2864.3	0.9466	0.9733	0.0014	0.0010
300	21.669	-2675.7	0.9723	0.9855	0.0010	0.0007
300	52.265	-2409.5	0.9882	0.9939	0.0007	0.0005
300	76.664	-2253.8	0.9928	0.9963	0.0005	0.0004
300	99.085	-2116.2	0.9958	0.9977	0.0004	0.0003
300	127.483	-1963.2	0.9972	0.9986	0.0003	0.0002
300	165.699	-1773.0	0.9987	0.9993	0.0002	0.0002
300	193.667	-1639.4	0.9991	0.9995	0.0002	0.0001